

# The $^{121}\text{Sb}(p,t)^{119}\text{Sb}$ Reaction at 21 MeV

P. Guazzoni, L. Zetta <sup>a</sup>, G. Graw, R. Hertenberg, H.-F. Wirth, and M. Jaskóla <sup>b</sup>

<sup>a</sup> Dipartimento di Fisica dell'Università and I.N.F.N I20133 Milano Italy

<sup>b</sup> Soltan Institute for Nuclear Studies Warsaw Poland

For the  $^{121}\text{Sb}(p,t)^{119}\text{Sb}$  reaction the measured differential cross sections display two kinds of shapes: one exhibit relevant angular structure, significant to allow a single  $L$  transfers to be distinguished, the others, rather featureless, originate from the incoherent superposition of several  $L$  transfers. Transferred angular momentum  $L$  has been assigned by comparing the shapes of the experimental angular distributions to DWBA calculations. Angular momentum transfers  $L$  and parities are assigned for all the 59 observed transitions. Generally we are able to fit the angular distributions of many observed transitions assuming only one  $L$  transfer. Eleven transitions display a quite smooth angular structure, distinctive of more  $L$  transfer contributions (see for example Fig. 1 and Fig. 2). These contributions have

been incoherently added with a weighting factor proportional to  $2L+1$  [1].

In table 1 the adopted energies, spins and parities of the  $^{119}\text{Sb}$  levels are presented in comparison with the results of the present work: the energies, the transferred angular momentum  $L$ , the spin and parity range, and the integrated cross sections from  $10^\circ$  to  $65^\circ$ . Our quoted energies are estimated to have an uncertainty of  $\pm 3$  keV. Absolute cross sections are estimated with a systematic uncertainty of  $\pm 15\%$  and reported with the statistical error.

## References

[1] J. Ball, Phys. Rev. **C6** (1972) 2139

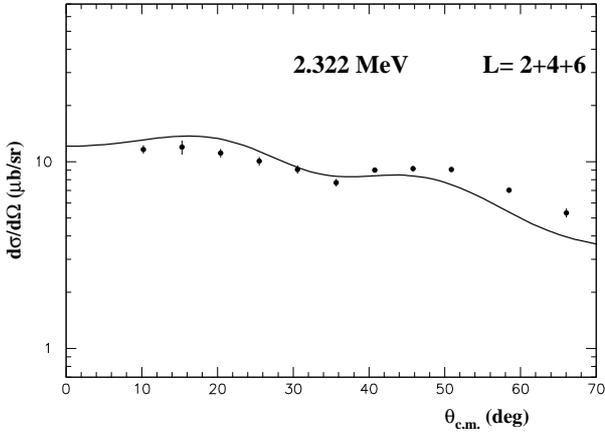


Fig. 1: Comparison between experimental and DWBA results

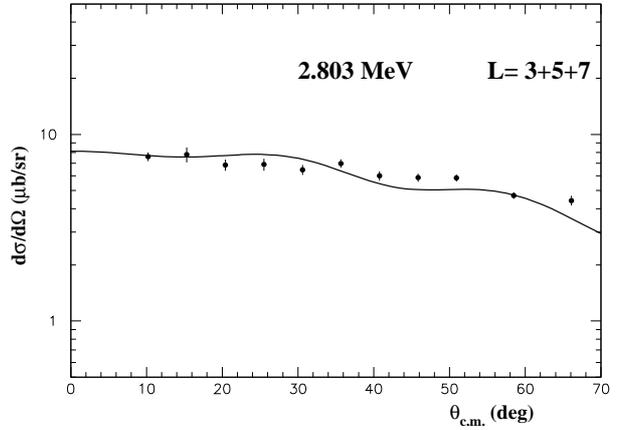


Fig. 2: Comparison between experimental and DWBA results

Table 1: Levels of  $^{119}\text{Sb}$

Adopted		Present experiment			
$E_{exc}$ (keV)	$J^\pi$	$E_{exc}$ (MeV)	$L_{tran}$	$J^\pi$	$\sigma_{int}$ ( $\mu\text{b}$ )
0.0	$5/2^+$	0.0	0	$5/2^+$	$2371 \pm 17$
270.52	$7/2^+$	0.271	4	$(3/2 - 13/2)^+$	$5.0 \pm 0.9$
644.03	$1/2^+$	0.644	2	$(1/2 - 9/2)^+$	$26 \pm 2$
699.88	$3/2^+, 5/2^+$	0.700	2	$(1/2 - 9/2)^+$	$8.8 \pm 1.2$
970.90	$9/2^+$				
1048.42	$7/2^+$	1.048	2	$(1/2 - 9/2)^+$	$149 \pm 5$
1212.74	$9/2^+$	1.213	2	$(1/2 - 9/2)^+$	$159 \pm 5$
1249.74	$9/2^+$	1.250	2	$(1/2 - 9/2)^+$	$29 \pm 2$
1327.25	$(1/2^-)$				
1338.61	$3/2^+$	1.334	2	$(1/2 - 9/2)^+$	$44 \pm 3$
1340.75	$11/2^+$				
1366.34	$11/2^-$	1.366	5	$(5/2 - 15/2)^-$	$29 \pm 2$
1407.35	$11/2^+$				
1413.21	$3/2^-$	1.413	3	$(1/2 - 11/2)^-$	$3.8 \pm 0.8$
1450					
1469	$3/2^+, 5/2^+$	1.469	2	$(1/2 - 9/2)^+$	$28 \pm 2$
1482	$1/2^-$				
1487.61	$(3/2^+)$				
1547					
1646.5	$1/2^+$				
		1.646	0	$5/2^+$	$25 \pm 1$
1660	$(7/2^+)$				
		1.662	2	$(1/2 - 9/2)^+$	$3.5 \pm 0.5$
1665	$(3/2^+, 5/2^+)$				

Adopted		Present experiment			
$E_{exc}$ (keV)	$J^\pi$	$E_{exc}$ (MeV)	$L_{tran}$	$J^\pi$	$\sigma_{int}$ ( $\mu\text{b}$ )
1675.72	13/2 <sup>+</sup>	1.675	4	(3/2 - 13/2) <sup>+</sup>	0.8± 0.2
1730		1.727	2	(1/2 - 9/2) <sup>+</sup>	1.7± 0.4
1749.64	3/2 <sup>+</sup>	1.750	2	(1/2 - 9/2) <sup>+</sup>	41± 2
1821.14	1/2 <sup>+</sup>	1.821	2	(1/2 - 9/2) <sup>+</sup>	3.0± 0.4
1848.2					
1875.32	(1/2 <sup>+</sup> , 3/2)	1.875	2	(1/2 - 9/2) <sup>+</sup>	5.3± 0.6
1970	7/2 <sup>+</sup> , 9/2 <sup>+</sup>	1.968	4	(3/2 - 13/2) <sup>+</sup>	2.0± 0.4
1982.0					
		2.019	4	(3/2 - 13/2) <sup>+</sup>	2.8± 0.4
2037.61	15/2 <sup>+</sup>				
		2.038	5	(5/2 - 15/2) <sup>-</sup>	3.4± 0.5
2043					
2067		2.068	4	(3/2 - 13/2) <sup>+</sup>	27± 1
2094.38		2.094	2+4+6	(7/2, 9/2) <sup>+</sup>	14± 1
2100					
2114	1/2 <sup>+</sup> , 3/2 <sup>+</sup> , 5/2 <sup>+</sup>	2.114	4	(3/2 - 13/2) <sup>+</sup>	12± 1
2129.82	9/2 <sup>-</sup>	2.130	3	(1/2 - 11/2) <sup>-</sup>	53± 2
2130					
2138.38	13/2 <sup>+</sup>	2.138	6	(7/2 - 17/2) <sup>+</sup>	3.0± 0.5
2159		2.162	3	(1/2 - 11/2) <sup>-</sup>	2.1± 0.4
2187		2.194	2+4+6	(7/2, 9/2) <sup>+</sup>	40± 2
2202.35	13/2 <sup>+</sup>	2.202	6	(7/2 - 17/2) <sup>+</sup>	11± 1
2223					
		2.232	3	(1/2 - 11/2) <sup>-</sup>	64± 2
2226.06	11/2 <sup>-</sup>				
2258					
2269.1	1/2 <sup>+</sup> , 3/2 <sup>+</sup> , 5/2 <sup>+</sup>				
2278.93	13/2 <sup>-</sup>				
2283.7	9/2 <sup>-</sup>	2.282	3	(1/2 - 11/2) <sup>-</sup>	19± 2
2298		2.294	2	(1/2 - 9/2) <sup>+</sup>	3.1± 0.4
2314.02	(15/2) <sup>-</sup>				
2320		2.322	2+4+6	(7/2, 9/2) <sup>+</sup>	33± 2
2327					
		2.339	3	(1/2 - 11/2) <sup>-</sup>	11± 1
2355					
2360.20	9/2 <sup>-</sup>				
2379.60	(9/2, 13/2)				
2384		2.380	2+4+6	(7/2, 9/2) <sup>+</sup>	22± 1
		2.403	3	(1/2 - 11/2) <sup>-</sup>	23± 1
		2.412	3+5+7	(9/2, 11/2) <sup>-</sup>	11± 1
2415.53	1/2 <sup>+</sup>				
2419.34	17/2 <sup>+</sup>	2.419	6	(7/2 - 17/2) <sup>+</sup>	2.4± 0.4
		2.448	0	5/2 <sup>+</sup>	13± 1
2455					
2475.44	15/2 <sup>-</sup>				
		2.475	3+5+7	(9/2, 11/2) <sup>-</sup>	8.2± 0.7
		2.490	4	(3/2 - 13/2) <sup>+</sup>	5.2± 0.6
2505.24	15/2 <sup>-</sup>				
2508		2.514	1	(3/2 - 7/2) <sup>-</sup>	17± 1
		2.527	0	5/2 <sup>+</sup>	33± 2
2539		2.539	2	(1/2 - 9/2) <sup>+</sup>	23± 1
2553.6	(19/2) <sup>-</sup>	2.554	3	(1/2 - 11/2) <sup>-</sup>	20± 1
2561					
		2.586	3+5+7	(9/2, 11/2) <sup>-</sup>	13± 1
2624		2.622	3+5+7	(9/2, 11/2) <sup>-</sup>	14± 1
		2.637	2	(1/2 - 9/2) <sup>+</sup>	11± 1
		2.670	3+5+7	(9/2, 11/2) <sup>-</sup>	15± 1
		2.687	3+5+7	(9/2, 11/2) <sup>-</sup>	7.3± 0.7
2707.74	17/2 <sup>-</sup>				
2708	1/2 <sup>+</sup> , 3/2 <sup>+</sup> , 5/2 <sup>+</sup>				
		2.728	2	(1/2 - 9/2) <sup>+</sup>	11± 1
2747.68					
2749					
		2.755	4	(3/2 - 13/2) <sup>+</sup>	6.1± 0.6
2769.08	(17/2 <sup>+</sup> )				
		2.777	3	(1/2 - 11/2) <sup>-</sup>	7.6± 0.7
		2.788	3	(1/2 - 11/2) <sup>-</sup>	8.2± 0.7
		2.803	3+5+7	(9/2, 11/2) <sup>-</sup>	23± 1
		2.815	9	(13/2 - 23/2) <sup>-</sup>	12± 1
		2.829	3	(1/2 - 11/2) <sup>-</sup>	5.2± 0.6
2841.7	(21/2) <sup>-</sup>				
2841.7	(27/2) <sup>+</sup>				
2848.99	19/2 <sup>+</sup>				
		2.849	5	(5/2 - 15/2) <sup>-</sup>	23± 1
2862					
		2.874	2	(1/2 - 9/2) <sup>+</sup>	7.5± 0.7
2885					